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February 22, 2010

WSA Engineering Ltd. 2248 Columbia Avenue Castlegar, BC V1N 2X1

Attention:

Ralf Waters, P. Eng.

Project Engineer

Dear Sirs:

Re:

VILLAGE OF SIVERTON – WATER WELL NO. 2 (WELL TAG 27023)

AOUIFER TESTING PROGRAM AND APPLICATION FOR IHA NEW

WATER SOURCE APPROVAL

1.0 INTRODUCTION

The present aquifer testing and water quality sampling program has been carried out by Aquilog Groundwater Monitoring Systems at the request of WSA Engineering Ltd. of Castlegar, BC on behalf of the Village of Silverton. The testing program was conducted with the Village of Silverton, Water Well No. 2, which was drilled in May, 2009. The new water well is constructed with 254 mm diameter casing, whereas the original well (Well No. 1) is constructed with 203 mm diameter casing. The new well is constructed with larger diameter casing and is designed to provide a higher well yield capacity with the purpose of meeting the greater water demands required during the summer months. A Construction Permit application was not filed at the time of construction of Water Well No. 2.

The main objective of the present testing program and accompanying report is two-fold as follows:

- 1. To evaluate the sustainable yield and water quality of the new groundwater source; and,
- 2. To file application for an IHA new water source approval.

The following report outlines the nature of the present program, provides a discussion of the findings along with a discussion of wellhead protection considerations. Report figures, field data including pumping test information and water quality data are attached to Appendices A, B and C. The Application for Construction Permit information is included in Appendix D.

2.0 BACKGROUND

The Village of Silverton is located on the east side of Slocan Lake, approximately 3.5 kms south of New Denver. The community of Silverton is situated on an alluvial fan/delta complex, which was built out into Slocan Lake as Silverton Creek downcut its present day course into the bedrock upland area.

In general terms, the alluvial fan is comprised of granular material ranging from cobbles and boulders to sand and gravel, mixed with varying proportions of silt and clay. The quantity and extent of silt and clay material, depends on the amount of fines carried by Silverton Creek during deposition and also, on the lake level when these sediments were laid down. During periods when the lake level was relatively high and flows within the creek were not excessively turbid, clean deposits of sand and gravel were deposited. These sand and gravel formations, because of their water transmitting capacity, form the major aquifers in this type of geologic setting.

Silverton's Well No. 1 was completed in May, 1988 under the supervision of Kala Groundwater Consulting Ltd. of Vernon, BC. It is a 203 mm diameter by 47.9 m deep well drilled by Owen's Drilling Ltd. of Cranbrook, BC. The total screen assembly is 6.4 m in length and this is comprised of four sections of Johnson's stainless steel well screen each 1.6 m in length (from top to bottom, a #30 slot, #40 slot, #15 slot and #40 slot). A 0.61 m riser pipe and Figure K packer is attached to the top of the screen assembly, bringing the top of the screen assembly to 40.8 m below ground level. A 24-hour aquifer test was conducted with the well pumping at a constant rate of 390 USgpm (24.6 L/s). Based on the test results, the well has a theoretical safe yield of approximately 1000 USgpm. However, the screens in Well No. 1 are designed to transmit 450 USgpm (28.4 L/s) at an entrance velocity of 0.1 feet per second and this was the recommended sustainable yield for the well. A copy of the driller's log and well completion diagram are attached to Appendix A of this report.

Well No. 2, the subject of this report, was completed in May, 2009 under the supervision of WSA Engineering Ltd. of Castlegar, BC. It is a 254 mm diameter by 47.5 deep well drilled by JR Drilling Ltd. of Cranbrook, BC. The new well is located 7.6 m downstream from Well No. 1. The total screen assembly in Well No. 2 is 6.1 m in length and is comprised of 3.3 m of #100 slot screen, 1.2 m of #40 slot and 1.8 m of #80 slot, 254 mm telescopic, stainless steel well screen. The well was developed by the air lift method for a period of approximately 10 hours. An evaluation of sustainable yield for Well No. 2 was one of the purposes of the present investigation and is discussed in Section 4 of this report.

3.0 FIELD PROGRAM

The field program was conducted during the period February 1 to February 3, 2010. All pump testing services were provided by Monashee Aquifer Testing of Lumby, BC, under the supervision of Larry C. Topp, P. Geo. with Aquilog Groundwater Monitoring Services.

The testing crew arrived on-site around mid morning, February 1, 2010 and met with Leonard Caisley, the contact person with the Village of Silverton. After becoming familiar with the well site conditions and proposed water discharge location for the pumping test, the crew started the program by conducting a down-the-hole camera inspection of Well No. 2. This was carried out to establish initial well depth soundings and water well completion details, including well screen settings. Following the camera work, a 30 HP test pump was set into the well to a depth of 38.1 m by the testing crew and the well was chlorinated. This was the end of day one.

On day two, Mr. Topp arrived on site at 8:00 AM with the water sample bottles obtained from Caro Analytical Services of Kelowna, BC on the previous day. The pump in Well No. 1 had been shut-down at around 12:00 midnight the previous night. After final preparation of the pumping test equipment, which included the laying of discharge line, installation of an orifice meter and a data logger in Well No. 2 the test was initiated. To start with a step-drawdown test was conducted involving three consecutive steps pumping at 153 USgpm (9.7 L/s), 302 USgpm (19.1 L/s) and finally 545 USgpm (34.4 L/s). After allowing the well to recovery for a 30 minute interval, the constant rate test was started at 10:30 AM, February 2, 2010. During the constant rate test the well was pumped at a continuous rate of 550 USgpm (34.7 L/s). Drawdown measurements were obtained manually from the production well (Well No. 2) and also drawdown interference was measured in Well No. 1 with an acoustic well sounder. In addition, water level drawdown was measured on a continuous basis in the production with the data logger.

At 8:00 AM on day three, the test crew was informed by Leonard that the reservoir level was starting to run low and asked if the test could be shut down a little earlier than the planned 24 hour pumping interval. Mr. Topp reviewed the test data and noted that the pumping level had stabilized during the night and in fact had recovered a small amount. Based on this, Mr. Topp recommended that the test could be shut down after all the water samples were obtained and following a short period of recovery measurements in the production well, the pump in Well No. 1 could be re-started. The test pump in Well No. 2 was shut-down at 8:30, which allowed a 22 hour pumping interval for the test and the pump in Well No. 1 was re-started at 8:45 AM.

It should be noted that during the pumping test with Well No. 2 a water quality profiling program between Silverton Creek and Well No. 2 was carried out on two separate occasions using a

Oakton Multi-Parameter Tester 35 field kit. The parameters included pH, temperature and conductivity.

4.0 PROGRAM FINDINGS

4.1 Aquifer Testing

A review of the DVD made during the down-the-hole camera inspection shows that after almost one year of the well sitting idle, some form of chemical precipitate has accumulated in the well screens. Judging by the color of the water (red) upon test start-up it would appear that this precipitate is iron oxide. A copy of the DVD can be obtained from Mr. L.C. Topp on request.

Results of the step-drawdown test are summarized in Table 1 following.

Table 1 – Specific Capacity Determinations						
Pumping Rate	Pumping Rate Specific Capacity after 30 mins pumpi					
153 USgpm	83.11 USgpm/m of dd					
302 USgpm	84.04 USgpm/m of dd					
545 USgpm	79.29 USgpm/m of dd					

With the exception of the final step the specific capacity remains fairly consistent throughout the step-drawdown test indicating that the well is efficient. The small decrease in specific capacity noted during the final step is not unusual and can be explained by the fact that the steps where run consecutively without a period of recovery between.

During the constant rate yield test, the pumping level showed a small decline (approximately 0.6 feet) for the first 540 minutes of pumping, which was followed by a stabilized pumping level between the 540 and 840 minute pumping interval and then the pumping showed a small rate of recovery during the final minutes of the pumping test.

The maximum amount of drawdown experienced during the 22 hour pumping test was 25.24 feet (7.69 m) which represents 39.4 % of the total available drawdown (TAD) in the well. TAD is defined as the distance between the static water level and the top of the well screen assembly, which in this case is 63.98 feet (19.5 m).

The sustainable yield for a water well is generally determined by extrapolating the rate of drawdown over an extended period of time (for example 5 or 20 years) and then projecting a pumping rate that will not exceed 70 percent of the total available drawdown. Applying this method, a sustainable yield projection for the subject water well would be in excess of 900

USgpm. We do not however recommend that the design production rate exceed the pumping test rate of 550 USgpm (34.7 L/s)

A second important factor to consider is that during the pumping test, the subject well produced sand. Even though the sand production was not excessive, it was noted on a continuous basis throughout the test. Sand production can present problems with pumping equipment, distribution lines and household fixtures. We would suggest that a program of further development be undertaken with this well. The general rule is that one hour of development is required for every foot of well screen in a large diameter water well. Well No. 2 has 20 feet of screen and has only been developed for 10 hours. An additional 10 hours of development may be required.

Two final observations relating to the pumping test phase of the program are; (a) the total drawdown interference measured in Well No. 1 (Observation Well) at the end of the pumping interval was 4.0 feet (1.22 m) and; (b) the water level in Well No. 2 (Pumping Well) recovered a full 99 % after only 15 minutes of shutting down the test pump.

4.2 Water Quality

At 8:30 AM on February 3.2010, near the end of the pumping test, water samples were obtained from Well No. 2 in properly prepared sampling bottles and transported immediately to Caro Analytical Services in Kelowna, BC for an extended potability analysis as per "HPF10160 Parameter List For New Drinking Water Sources". Certificates of analysis are provided in Appendix C of this report. A brief characterization of the raw water quality from Well No. 2 is as follows:

Microbiological Parameters – Based on the water samples obtained on February 3, 2010, Total Coliforms, Background Colonies and E. Coli were all below the detection limits. Iron related bacteria and Sulfate reducing Bacteria were <2 and <8.0 respectively, both below the detection limits.

General Parameters - All parameters for which an analyses was performed fall within the Guidelines for Canadian Drinking Water Quality (GCDWQ).

Total Recoverable Metals by ICPMS - All parameters for which an analyses was performed fall within the Guidelines for Canadian Drinking Water Quality (GCDWQ).

UV Transmittance - The UV Transmittance @ 254mm was 97.5.

In general terms the water may be characterized as moderately soft and of excellent quality.

5.0 WELLHEAD PROTECTION CONSIDERATIONS

The Village of Silverton's production wells (Well No. 1 – Well Tag 66073 and Well No. 2 – Well Tag 27023) are located approximately 25 m southeast of Silverton Creek and are separated by a distance of approximately 7.9 m. A site plan and ortho-mosaic photo is shown in Figure 1 and 2 respectively (see Appendix A).

There are no MOE website Aquifer Vulnerability Maps available for this area at this particular time and therefore aquifer vulnerability cannot be defined in this manner. We did however consider some other factors including lithology, water levels and water quality profiling between the creek and the wells. A review of the lithologic profile for Water Well No. 1 indicates that the silty to clayey sand and gravel encountered between 12 and 136 feet (3.7 and 41.5 m) below ground surface will provide and excellent filtering media and protective zone above the aquifer. The top of the aquifer was encountered at 136 feet (41.5 m) below ground surface. Secondly the static water level in Well No. 2 is 66.52 feet (20.27m), whereas the water level in the creek is approximately 15 feet (4.5 m) below ground surface, indicating that there is no direct hydraulic connection between Silverton Creek and the well field. Finally results of the water quality profiling taken between the creek and Well No. 2 is summarized in Table 2 following.

Table 2 - Water Quality Profiling Summary								
Feb. 2, 2010 @ 1445 hrs Feb. 3, 2010 @ 0810 hrs								
Well No. 2	Creek	Well No. 2	Creek					
pH: 7.8	pH: 8.0	pH: 7.4	pH: 8.1					
Cond: 158	Cond: 155	Cond: 179	Cond: 155					
Temp: 6.7 C	Temp: 3.3 C	Temp: 6.9 C	Temp: 3.0 C					

Even though the profile differences are not significant, the findings do provide evidence that there is not a direct hydraulic connection between the Creek and Well No. 2. Also the minor changes that did occur between the two sets of readings, were in opposite directions. Taking all factors into consideration, including water quality, there is more evidence to support a NON-GWUDI source of water supply as opposed to a GWUDI source.

Generally the Capture Zone for an aquifer of this nature will be relatively narrow (probably less than 20 m in width), will not extend too far downstream (less than 5 m), but may extend a fair distance upstream, depending on the extent and nature of the sand and gravel deposit. This would suggest that all future wellhead protection efforts be concentrated in an upstream direction.

The nearest sewage disposal system located upstream of the well field is situated approximately 45 m away, which is outside of the 30 m criteria. We would recommend that the Village place restrictions on the number and location of any future septic systems.

There is one light industrial complex located further upstream of the well field and we would suggest that the Village insist that any fuel storage tanks associated with this complex have proper containment structures. For example they should be placed on a cement pad, constructed with raised berms around the perimeter.

6.0 CONCLUSIONS AND RECOMMENDATIONS

Based on the results of the present aquifer testing and water sampling program, the following conclusions and recommendations are provided for Client/Approving Authority considerations.

- The testing program was conducted with the Village of Silverton, Water Well No. 2, (Well Tag 27023), which was drilled in May, 2009. The water source is a 254 mm diameter by 47.7 m deep drilled water well located approximately 7.9 m southwest of the original Water Well No. 1.
- The main objective of the present testing program and accompanying report is two-fold as follows:
 - o To evaluate the sustainable yield and water quality of Well No. 2, and;
 - o To file application for an IHA new water source approval.
- The Village of Silverton is located on the east side of Slocan Lake, approximately 3.5 kms south of New Denver. The community at Silverton is situated on an alluvial fan/delta complex, which was build out into Slocan Lake as Silverton Creek downcut its present day course into the bedrock upland area.
- The field program, carried during the period February 1 to February 3, 2010, involved a down-the-hole camera inspection of Well No. 2, a step-drawdown test followed by a 22 hour constant rate pumping test, the collection of water samples as per HPF10160 parameter list, and water quality profiling between Silverton Creek and Water Well No. 2.
- The specific capacity of Well No. 2 based on the results of the step-drawdown test ranged from 83.11 USgpm/m of drawdown while pumping at 153 USgpm, declining to 79.29 USgpm/m of drawdown while pumping at 545 USgpm.
- The maximum amount of drawdown experienced during the 22 hour pumping test was 25.24 feet (7.69 m) which represents 39.4 % of the total available drawdown (TAD) in the well.
- A sustainable yield projection for the subject water well would be in excess of 900 USgpm. We do not however recommend that the design production rate exceed the pumping test rate of 550 USgpm (34.7 L/s).
- With respect to water quality all parameters for which an analyses was performed meet the Guidelines for Canadian Drinking Water Quality and overall the quality could be characterized as excellent.
- During the pumping test, Water Well No. 2 produced a small amount of sand, but on a continuous basis. We are recommending additional development of the well.
- Taking all factors into consideration, including water quality, there is more evidence to support a NON-GWUDI source of water supply as opposed to a GWUDI source.

7.0 CLOSURE

This report was prepared in accordance with generally accepted hydrological evaluation practices. The applicability of this report is only valid to the extent that there has been no material alteration from any of the said descriptions provided to Aquilog Groundwater Monitoring Systems (AGMS), unless AGMS is specifically requested by the client to review and revise this report in light of such alterations. This report must be used in its entirety. Statements of professional opinion are those of AGMS. If additional information or assessment findings arise which may alter the conclusions and/or recommendations of this report AGMS would be pleased to review and append our report where required.

We trust this meets your present requirements and if there are any questions or concerns regarding the investigation, please do not hesitate to contact the undersigned at (250) 549-0704

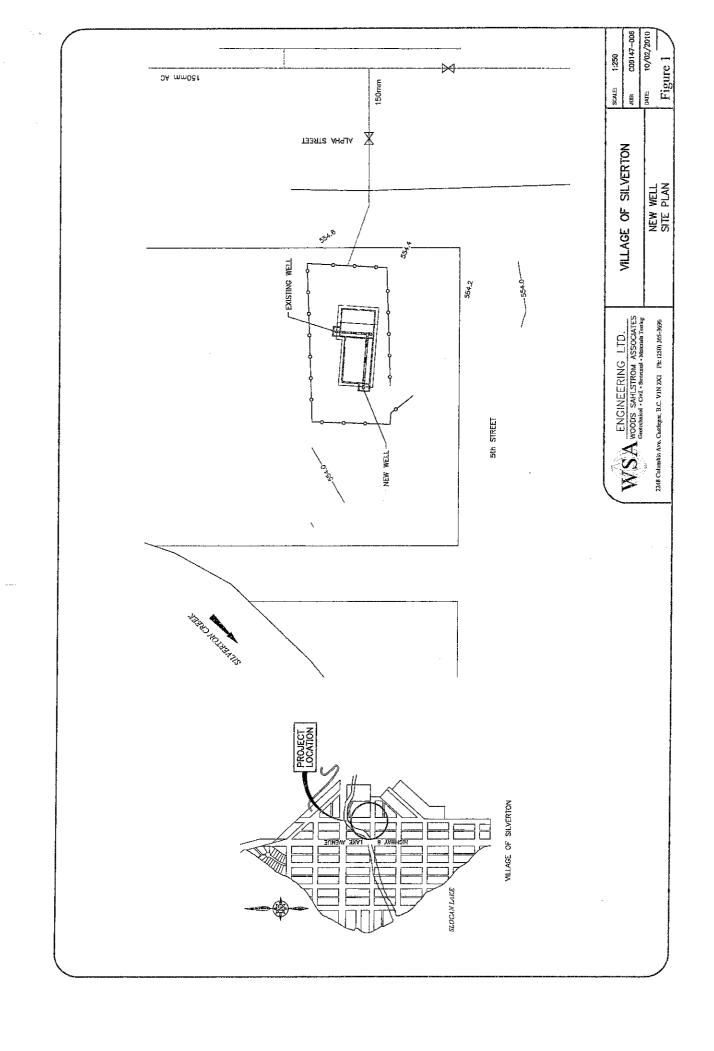
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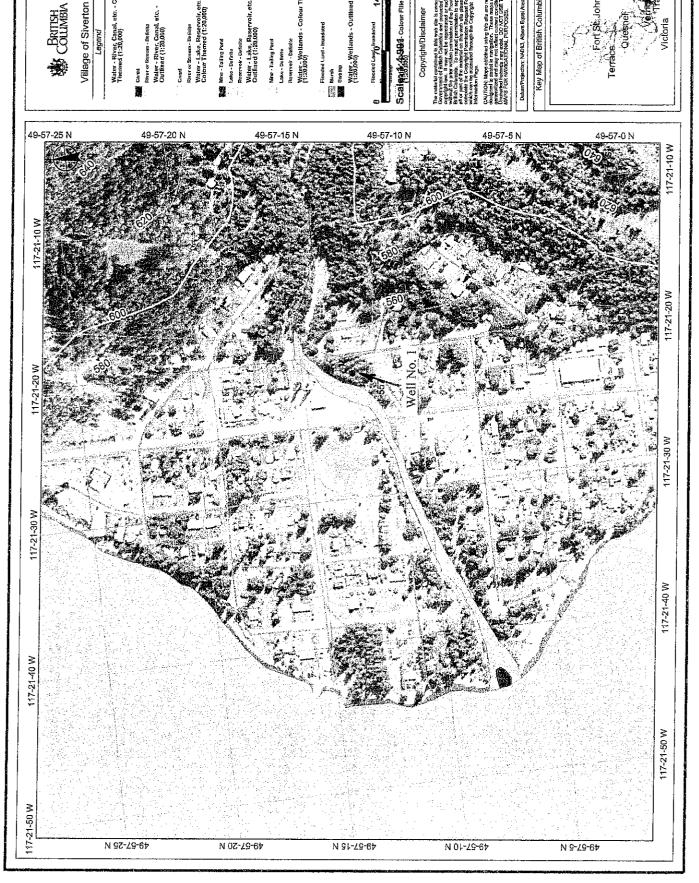
Aquilog Gracific Water Monitoring Systems

Hydrogeologist

APPENDIX A

- Report Figures
 Lithology and Well Completion (Wells 1 and 2)
 Site Photos





VILLAGE OF SILVERION TEST/PRODUCTION WELL DRILLER'S LITHOLOG

Depth Interval in feet	Lithologic Description
0 - 4 $4 - 12$ $12 - 16$	Silty sand and gravel with cobbles Boulders, up to 3 feet diameter Silty sand and gravel with cobbles
16 - 33 33 - 57	and boulders Silty sand with gravelly zones Silty gravel, grey, moist
57 - 80 80 - 95	Silty gravel with lenses of silty sand Gravel with silt and silty clay, wet
95 - 98 98 - 117	Silty sand with gravel, moist Silty gravel, loose intervals, wet
117 - 119 119 - 136	Silty clay, grey Clayey silt with gravel, wet
136 - 148	Sand and gravel, water-bearing, material grading from fine sand to med. gravel
148 - 151 151 - 158	Sand with some gravel Sand and gravel

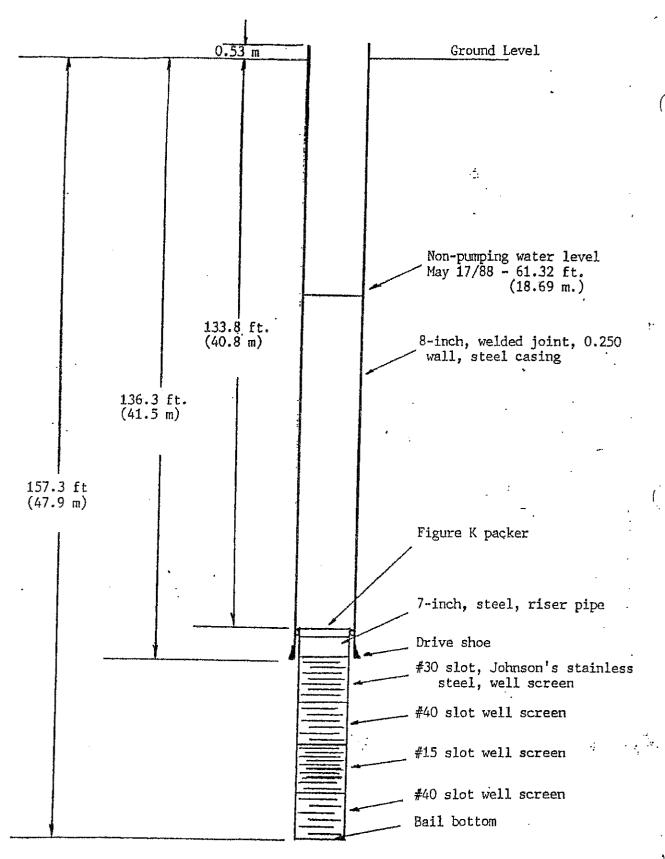


FIGURE 2 WELL COMPLETION DIAGRAM

Identify Results

Well ID:

Coordinate Position BC Albers: 1618832, 586446 Geographic: 49° 57' 12.8" N, 117° 21' 21.3" W UTM 11N: 474466, 5533528 Well Lithologies Well Tag No.: 000000066073 Source Accuracy: Feature Code: WA12100190 Lithology Description ID: 285580 Well ID: 66722 Lithology Sequence Number: 0 Lithology From: Lithology To: 15 Lithology Raw Data: **GRAVEL CLAY & BOULDERS** AREA: LEN: Well Tag No.: 000000066073 Source Accuracy: G Feature Code: WA12100190 Lithology Description ID: 285581 Well ID: 66722 Lithology Sequence Number: 0 Lithology From: 15 Lithology To: 130 Lithology Raw Data: HARDPAN SAND & GRAVEL AREA: LEN: Well Tag No.: 000000066073 Source Accuracy: G Feature Code: WA12100190 Lithology Description ID: 285582 Well ID: 66722 Lithology Sequence Number: 0 Lithology From: 130 Lithology To: 136 Lithology Raw Data: WET SANDY CLAY AREA: LEN: 0 Well Tag No.: 000000066073 Source Accuracy: Feature Code: WA12100190 Lithology Description ID: 285583 Well ID: 66722 Lithology Sequence Number: 0 Lithology From: 136 Lithology To: 146 Lithology Raw Data: SAND & GRAVEL AREA: 0 LEN: 0 Well Tag No.: 000000066073 Source Accuracy: G Feature Code: WA12100190 Lithology Description ID: 285584

66722

Lithology Sequence Number: 0 Lithology From: 146 Lithology To: 154

Lithology Raw Data: COURSE AND FINE SAND

AREA: 0

Well Tag No.: 000000066073

Source Accuracy: G

Feature Code: WA12100190 Lithology Description ID: 285585 Well ID: 66722

Lithology Sequence Number: 0 Lithology From: 154 Lithology To: 159

Lithology Raw Data: SAN & GRAVEL

AREA: 0 LEN: 0



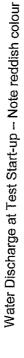
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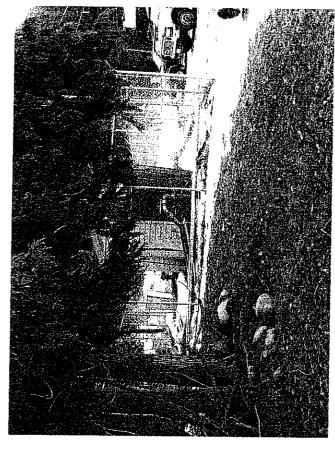
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Ministry Well ID Plate Number: 27023
Ministry Well Tag Number:

Cl Confirmation/atternative specs, attached
Cl Original well construction report attached

Uwner name: VILLAGE OF SILVERO Mailing address:	
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Lithologic description (see notes 6-13) or closure description	(see notes 14 and 15)
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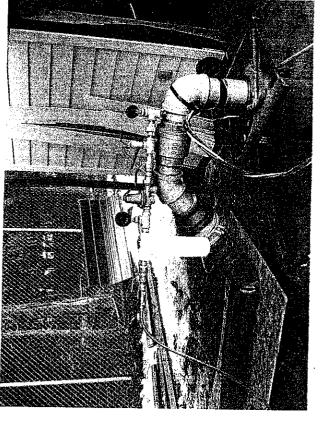




Well Field Compound Showing Water Well No. 1 and 2

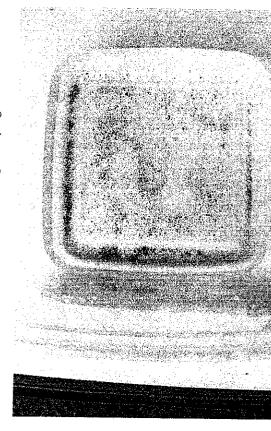


Measuring Water Level Drawdown During Pumping Test

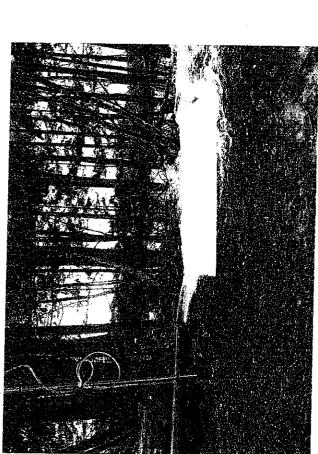


Wellhead Configuration During Pumping Test

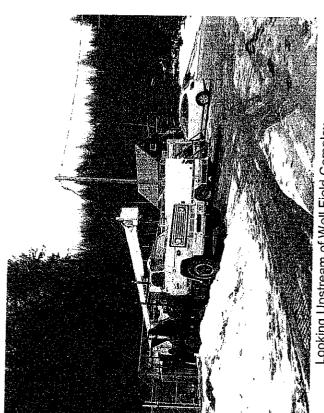
Water Discharge After 5 hours of Pumping (Water Clear)



Some of the Sand Pumped During the Aquifer Test



Looking Upstream of Well Field Complex



APPENDIX B

- Pumping Test Data

PUMPTEST (Drawdown)

Village of Silverton

Water Well No. 2 (Well Tag 27023) - Step Drawdown Test

Date test started: Feb. 2, 2010

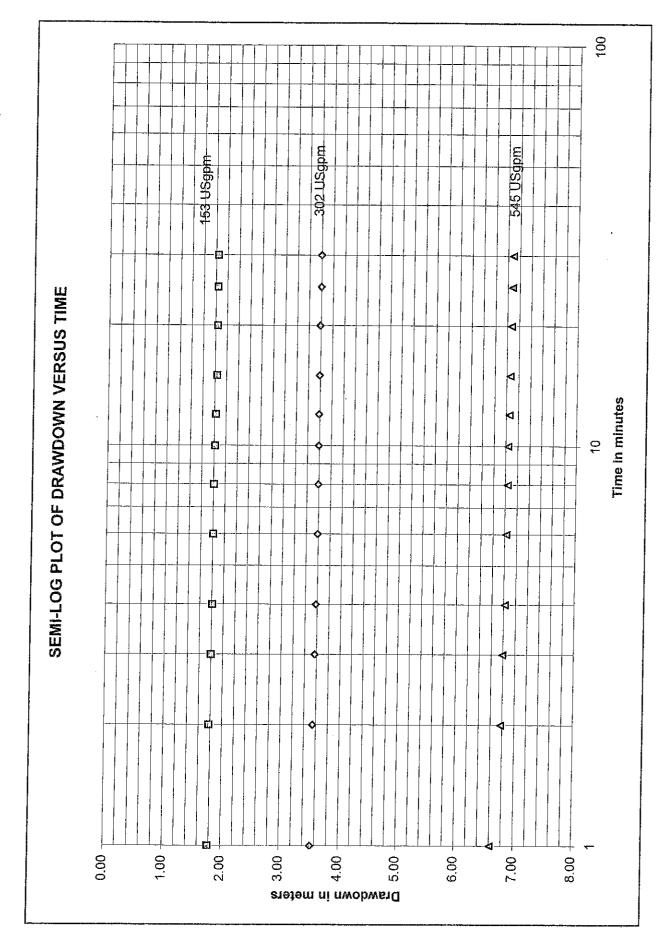
Time test started: 8:30 AM

Ave: pumping rate: See Comments Pre-test water level: 20.88 meters Reference Point: Top of Casing

Height of ref. point: 0.61 m above ground

Depth of well: 47.7 m
Top of screen: 39.8 m

Time (t) since	Depth to	Drawdown	,
pumping started in minutes	water in feet	in feet	Comments
Step No. 1 - 153 USgp	m		
1	22.66	1.78	Pumping rate: 153 USgpm
2	22,66	1.78	5.5-inches on 4-inch orifice plate
3	22.68	1.80	
4	22.69	1.81	
6	22.69	1.81	
8	22.69	1.81	
10	22.70	1.82	
12	22.71	1.83	
15	22.72	1.84	
20	22.72	1.84	
25	22.72	1.84	
30	22.72	1.84	
Step No. 2 - 302 USgpi	m		
1	24.41		
2	24.43	3.55	Pumping rate: 302 USgpm
3	24.45	3.57	21.5-inches on 4-inch orifice place
4	24.46	3.58	
6	24.47	3.59	
8	24.47	3.59	
10	24.47	3.59	
12	24.47	3.59	
15	24.47	3.59	
20	24.47	3.59	
25	24.48	3.60	
30	24.48	3.60	
tep No. 3 - 545 USgpn	, 		
1	27.49	6.61 F	Pumping rate: 545 USgpm
2	27.65		70 inches on 4-inch orifice plate
3	27.67	6.79	
4	27.70	6.82	
6	27.71	6.83	
8	27.72	6.84	
10	27.72	6.84	,
12	27.73	6.85	
15	27.74	6.86	
20	27.75	6.87	
25	27.76	6.88	
30	27.77	6.89	



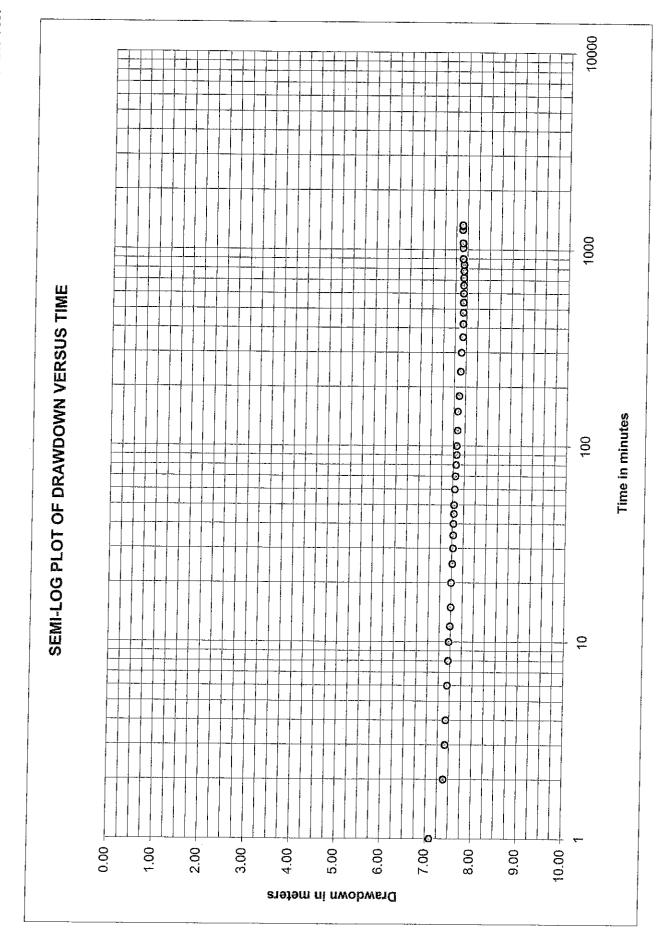
Aquilog Groundwater Monitoring Systems

Village of Silverton Water Well No. 2 - Well Tag 27023 PUMPTEST (Drawdown)

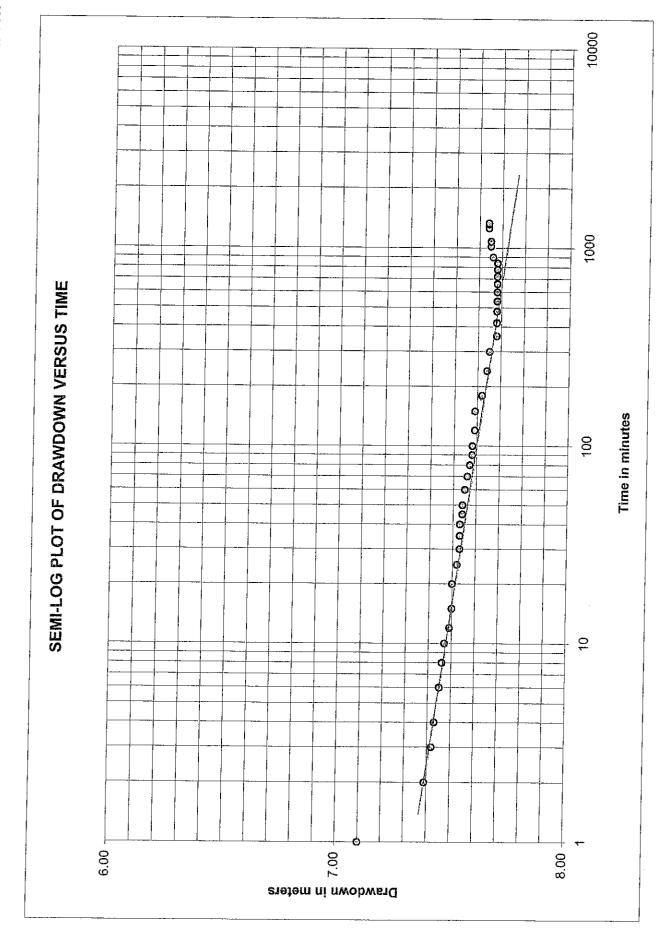
Date test started: Feb. 2, 2010 Time test started: 10:30 AM Ave. pumping rate: 550 USgpm Pre-test water level: 20:88 meters Reference Point: Top of casing Height of ref. point: 0.61 m above ground

Depth of well: 47.7 m Top of screen: 39.8 m.

Time (t) since	Depth to	Drawdown	
pumping started in minutes	water in feet	in feet	Comments
0	20.88	0.00	
1	27.98		Pumping rate: 550 USgpm (34.7 L/s)
2	28.27	7.39	19.5 inches on 5-inch orifice plate
3	28.30	7.42	
4	28.31	7.43	
6	28,33	7.45	
8	28.34	7.46	
10	28.35	7.47	
12	28.37	7.49	
15	28.38	7.50	
20 25	28.38 28.40	7.50 7.52	
30	28.41	7.52 7.53	
35	28.41	7.53	
40	28.41	7.53	
45	28.42	7.54	
50	28.42	7.54	
60	28.43	7.55	
70	28.44	7.56	
80	28.45	7.57	
90	28.46	7.58	
100	28.46	7.58	
120	28.47	7.59	
150	28.47	7.59	
180	28.50	7.62	
240	28.52	7.64	
300	28.53	7.65	
360 420	28.56	7.68	
480	28.56 28.56	7.68 7.68	
540	28.56	7.68	
600	28.56	7.68	
660	28.56	7.68	
720	28.56		Pumping rate remained constant at 550 USgpm throughout test
780	28.56	7.68	Target of the control
840	28.56	7.68	
900	28.54	7.66	
1020	28.53	7.65	
1080	28.53	7.65	
1260	28.52	7.64	
1320	28.52	7.64	
1335	28.52	7.64	Water samples obtained at 8:45 AM on Feb. 3, 2010
	~		
<u> </u>			
···			



Aquilog Groundwater Monitoring Systems



Aquilog Groundwater Monitoring Systems

PUMPTEST (Drawdown) Village of Silverton - Well No. 1 (Obs. Well) Used as Observation Well during Pumping Test with Well No. 2

Date test started: Feb. 2, 2010 Time test started: 10:30 AM

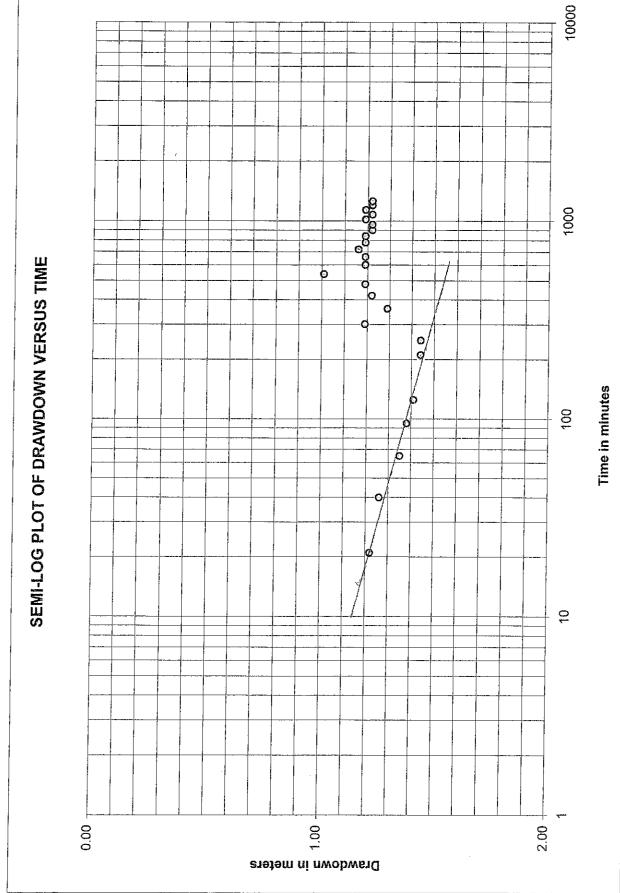
Ave. pumping rate: 550 USgpm Pre-test water level: 21:36 meters Reference Point: Top of casing

Height of ref. point: 0.61 m above ground

Depth of well: 47.9 m Top of screen: 40.8 m

Pre-test water level:	21.36 meters		Top of screen: 40.8 m
Time (t) since	Depth to	Drawdown	
pumping started in minutes	water in feet	iñ féet	Comments
0			
21	22.58		Pumping rate: 550 USgpm (34.7 L/s) in Well No. 2
40 65		1.26	19.5 inches on 5-inch orifice plate
95	22.71 22.74	1.35	
125	22.74	1.38 1.41	
211	22.80		
250	22.80		
302	22.55	1.19	
361	22.65	1.29	
421	22.58	1.22	
481	22.55	1.19	
541	22.37	1.01	
602	22.55	1.19	
661	22.55	1.19	
721	22.52	1.16	
781	22.55	1.19	
841	22.55	1.19	
901	22.58	1.22	
961	22.58	1.22	
1021 1081	22.55	1.19	
1141	22.58 22.55	1.22	
1201	22.58	1.19	
1261	22.58	1.22 1.22	
1201	22.00	1.22	
	-		
wilde Groundwater ma		= ~	

Village of Silverton



Aquilog Groundwater Monitoring Systems

MONASHEE AQUIFER TESTING BOX 752, LUMBY,B.C. VOE 2G0 250-547-6845

PUMP TEST - DRAWDOWN DATA

PAGE OF

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Datum	Point .	<u> </u>				f Datum Poin		om Ground Level	
		evel	Jan 1	<u> </u>	Total Draw	down <u>O S</u>	34	TAD 64.03 Dm.211119ke @ 125: Sc	ROTAL W
	<u> Сэћ</u> ме	ELAPSED TIME SINCE PUMPING STARTED	ELAPSED TIME SINCE PUMPING STOPPED	RATIO (t/t')	DISTANCE TO WATER	nesedual DRAWDOWN		REMARKS	
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	38	23			7446	5 94			
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	42	12			74.51	5,99			
08	45	15			74 53	6.01			
<u></u>	50	20			7453	I .			
	55	Ø5			74.55				
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	50	30			80 6	V. 64		al,5" of head	
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	08	38			80.08	1.76			
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					1 3 30	78			
	<u> </u>				13/31	11.79			

MONASHEE AQUIFER TESTING BOX 752, LUMBY, B.C. VOE 2G0 250-547-6845

PUMP TEST - DRAWDOWN DATA

PAGE S OF

TIED TEST

2010 HTNOM YEAR DAY

PROJECT VIllage Of Salverton 21 Grown Ground _____ Elevation of Datum Point _ Datum Point ___ ______ Total Drawdown Static Water Level ____ Level 68 50 MODADENO ProTest DISTANCE ELAPSED REMARKS ELAPSED RESIDUAL RATIO TIME SINCE TO TIME SINCE DRAWDOWN PUMPING (t/t') TIME PUMPING WATER STOPPED STARTED 5/15 USGRM 7,0"05 head t' (min.) t (min.) MIN, HR. 11791 (a)09 9168 3 22.19 22.26 2,2, 24 24 (04 aa 35 90 22.40 35/2 66 40 37 29.42 كرت 6 39 gg . 48 95 (59 29 22.44 96 40 92 20 46 45 99 SI Q_{i}^{\perp} 09 45 Q99 54 0 22.56 55 85 90 10

PUMP TEST - RECOVERY DATA STEP TEST

PAGE 3 of 4

PROJECT VIlleye of Silverson 9010 DAY MONTH YEAR No 2 Well Tag Ma 27083 Elevation of Datum Point ______ Datum Point .___ 59 Total Drawdown 22 <u>68 52</u> Plimo intake Yro Test ruel ELAPSED TIME SINCE ELAPSED DISTANCE RESIDUAL RATIO TIME SINCE REMARKS TO TIME (t/t') DRAWDOWN PUMPING PUMPING WATER STOPPED STARTED t' (min.) HR. MIN. t (min.) . . 1 22 59 90 10 00 00 . 95 67.47 3050 68.75 123 01 CY! 01 .16 68.38 ()1,3052 93 12 02 X) 3054 0.2 03 113 6835 03 3054 61. 09 M , 12 /H 3050 11. 05 68,63 11 06 68.52 : 10 07 69 62 (11) 08 09 68.62 .10 .10 10)) .09 19 .09] <= 10,80 10 .08 90 107 25 68 58 2 106

NO. 340-L410 DIETZGEN GRAPH PAPER
SEMI-LOGARITHMIC
4 CYCLES X 10 DIVISIONS PER INCH

DIETZGEN CORPORATION

MONASHEE AQUIFER TESTING BOX 752; LUMBY, B.C. VOE 2G0 250-547-6845

710

PUMP TEST - DRAWDOWN DATA 24 HR

PAGE OF

PROJECT VILLOGE OF TIMER FOR MONTH YEAR DAY Elevation of Datum Point 2 from Ground Leve Datum Point ____ Total Drawdown . Safe TRI 60,40 macco (Well NO I Shot down) PUMS HO TOSIN Leve ELAPSED DISTANCE ELAPSED -INTEST DIOWER RATIO TIME SINCE REMARKS TIME SINCE TO TIME PUMPING (t/t') DRAWDOWN PUMPING STOPPED WATER STARTED t' (min.) t (min.) HR. MIN. 20-60 550 VS689 30 O(0)17 -6" or fice were 281 $Q \setminus P_1 C$ 23 24.23 32 24 86 33 14 . 3(a .88 24 QA 4Q 94 20 24 A3 26 20 46 ΦQ 27 14 AO 92 98 29 34.4h 92 q<u>ş</u> 251 93 24 49 co. JA F.F. Q'3 J4.58 45 \bigcirc 2 3 (3 84.61 CLACKOR LOW 00 1,9 \$ 1 $\circ\circ$ 30 69 $\rho_{\rm G}$ 35 05 0 1 10 15 20 50 $\Delta \mathbb{C}$ 16 30 (n0)4(). J () L F 1 80 186 13 (50 9() J8 1 2 00/ 10 177 1/0 20 34 38 190 OF P. jQ, 49 150 00 24 98 TOURS HOO 93.50 30 180 .59. 可利用項 00

MONASHEE AQUIFER TESTING BOX 752, LUMBY,B.C. VOE 2GO 250-547-6845

PUMP TEST - DRAWDOWN DATA

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Static Water Level 70 70]	Total Drawdown 25 05' TOTO 104 03' Kins 1070 Ke 0 125' 50 12 70 100 40							
ELAPSED ELAPSE TIME SINCE TIME SIN TIME PUMPING PUMPIN		68 ELAPSED TIME SINCE PUMPING STOPPED	RATIO (t/t')	DISTANCE TO WATER	RESIDUAL DRAWDOWN	1 KC () :c	REMARKS	7304				
HR.	MIN.	t (min.)	t' (min.)									
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<u> </u>	30	660			93.70	25 99						
30	30	7.20			1370	35 30		Checken nello				
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MONASHEE AQUIFER TESTING BOX 752, LUMBY, B.C. V0E 2G0

PUMP TEST - RECOVERY DATA

. PAGE 3 OF A

PROJECT 11 ONE OF COLECTOR MONTH YEAR DAY Elevation of Datum Point Trans Groupe Fove Datum Point ___ Total Drawdown <u>05</u> Static Water Level _____/___ 10/000 a トとりて ELAPSED ELAPSED DISTANCE RATIO RESIDUAL TIME SINCE TIME SINCE REMARKS TO TIME DRAWDOWN PUMPING PUMPING (t/t') WATER STOPPED STARTED t' (min.) HR. MIN. t (min.) -30 35 1335 00 27 1336 o∂ -jū $\sqrt{2g} \sin \phi$ - - 0 1242 19 110 2 1)) Or & or W 11.0(017:00 c

Static hevel Well tag the 27023

Well tag the 27023

Well no #2 70.72 <u>ک</u> NO. 340-L410 DIETZGEN GRAPH PAPER
SEMI-LDGARITHMIC
4 CYCLES X 10 DIVISIONS PER INCH DIETZGEN CORPORATION 7440 9 4 8 6 0

MONASHEÈ AQUIFER TESTING BOX 752, LUMBY,B.C. V0E 2G0 250-547-6845

PUMP TEST - DRAWDOWN DATA

PAGE 1B OF 2

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PROJE	ст Уу	1100 B S	<u> </u>	<u> </u>	1	I.s.		DAY	MONTH	YEAR
Vell _	1/0			1400 40	Kiri Mo					
) Datum	Point .	<u> </u>				f Datum Point			<u> </u>	
		evel	70.1′	<u>Acoustic</u> Soucce	Total Draw	down				
T1	ME	ELAPSED TIME SINCE PUMPING STARTED	ELAPSED TIME SINCE PUMPING STOPPED	RATIO (t/t')	DISTANCE TO WATER	RESIDUAL DRAWDOWN		R	EMARKS	
HR.	MIN.	t (min.)	t' (min.)	, de la companya de l	701/			<u>,</u>		
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16	31	261			74.3					
10	131	1. 8 F/ 1			74 1					
18	31				74.0					
19	31				73.4					
20	32				74.0					
	13.1				74.0					- Marine je somernin Cl

PUMP TEST - RECOVERY DATA

PAGE 2^8 OF 2

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PROJE	ст 1	illage	0 f c	Silve	rton			O A	<u>OA</u>	/ O YEAR
Well _	11)	1		Monito	- <u> </u>	We//_		<u></u>		
		TAR			_					
Static \	Water L	evel 70	1 Acou	under	Total Draw	down			·	
	ME	PUMPING STARTED	PUMPING STOPPED	RATIO (t/t')	DISTANCE TO WATER	RESIDUAL DRAWDOWN		RE	MARKS	
HR.	MIN.	t (min.)	t' (min.)							
22	31	720			73.9					
23	31	780			74.0					
<u> </u>	3/	R-40			74.0					
0/	3	900			74.1					
02	3/				74.1					
03	31	1020			74.0				•	
04	3/				74.1					
05	3/	112			74.0					
06	3/				74.1					
7	3/	1260			74.1					
				CONTROL OF THE STREET OF THE S	Sangled professionary Sample of Artifester Warry Street Cat garages.	Particular and State of Control of the Control of t	AND THE PROPERTY OF THE PROPER	aggino de poet y <u>all</u> Laftin la paine et glandad glandad per canada la	The art years and by any output account of the art of t	ggyk, deur S.VII Het TS.VII Hygings
\bigcirc 9	00				76.4	Pump	0+1			
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·										

APPENDIX C

Water Qulaity Data

CERTIFICATE OF ANALYSIS



CLIENT

Topp, Larry

114 - 6688 Tronson Road

Vernon BC

V1H 1R9

1"EL

1-250-549-0704

FAX

ATTENTION

Larry Topp

RECEIVED / TEMP

Feb-03-10 14:55 / 2.0 °C

WORK ORDER

K0B0153

REPORTED

Feb-15-10

PROJECT

Silverton Well #2

COC #(s)

26688

PROJECT INFO

Well #2, Tag 27023

General Comments:

CARO Analytical Services employs methods which are based on those found in "Standard Methods for the Examination of Water and Wastewater", 21st Edition, 2005, published by the American Public Health Association (APHA); US EPA protocols found in "Test Methods for Evaluating Solid Waste, Physical/Chemical Methods, SW846", 3rd Edition; and protocols published by the British Columbia Ministry of Environment (BCMOE).

Methods not described in these publications are conducted according to procedures accepted by appropriate regulatory agencies, and/or are done in accordance with recognized professional standards using accepted testing methodologies and quality control efforts except where otherwise agreed to by the client.

The results in this report apply to the samples analyzed in accordance with the chain of custody document. This analytical report must be reproduced in its entirity. CARO is not responsible for any loss or damage resulting directly or indirectly from error or omission in the conduct of testing. Liability is limited to the cost of analysis. Samples will be disposed of 30 days after the test report has been issued unless otherwise agreed to in writing.

- · All solids results are reported on a dry weight basis unless otherwise noted
- Units:

 $mg/kg = milligrams \ per \ kilogram, \ equivalent \ to \ parts \ per \ million \ (ppm)$

mg/L = milligrams per litre, equivalent to parts per million (ppm) ug/L = micrograms per litre, equivalent to parts per billion (ppb) ug/g = micrograms per gram, equivalent to parts per million (ppm)

ug/m3 = micrograms per cubic meter of air

"RDL"

Reported detection limit

• "<^{1t}

Less than reported detection limit

• "AO"

Aesthetic objective

"MAC"

Maximum acceptable concentration (health-related guideline)

"LAB"

RMD = CARO - Richmond location, KEL = CARO - Kelowna location, SUB = Subcontracted

Please contact CARO if more information is needed.

CARO Analytical Services

Final Review Per:

Ed Hoppe, B.Sc, P.Chem

Laboratory Manager

CARO Analytical Services (Kelowna)

102 - 3677 Highway 97N Kelowna, BC Canada V1X 5C3

Tel; (250) 765-9646 Fax: (250) 765-3893 Web: www,caro.ca

SAMPLE DATA



CLIENT PROJECT FILE Topp, Larry Silverton Well #2 WORK ORDER #
REPORTED

K0B0153 Feb-15-10

Analyte	Result	Canadian DW Guidelines	RDL	Units	Analyzed	Method	Lab	Notes
		(May 08)						

General Parameters

Silverton Well# 2, (Well Tag 27023)	(KOBO153-01)	Matrix: Water	Sampled: Feb	-03-10 08:3	10		
Aggresiveness Index	11.4			-	Feb-12-10	Reference	KEL
Alkalinity, Total as CaCO3	70.4		1.0	mg/L	Feb-04-10	APHA 2320 B	KEL
Carbon, Total Organic	0.8		0.5	mg/L	Feb-05-10	APHA 5310 B	KEL
Chloride	0.51	AO ≤ 250	0.10	mg/L	Feb-04-10	APHA 4110 B	KEL
Colour, True	<5	AO ≤ 15	5	Color Unit	Feb-05-10	APHA 2120 B	KEL.
Conductivity (EC)	172		5	uS/cm	Feb-04-10	APHA 2510 B	KEL
Cyanide (total)	< 0.01	MAC = 0.2	0.01	mg/L	Feb-10-10	APHA 4500-CN	KEL.
Fluoride	0.11	MAC = 1.5	0.10	mg/L	Feb-04-10	APHA 4110 B	KEL
Hardness, Total (Total as CaCO3)	81.3		2,91	mg/L	Feb-09-10	APHA 2340 B	RMD
Langelier Index	-0.73		-5.0	-	Feb-12-10	Reference	KEL
Nitrogen, Ammonia as N	<0.02		0.02	mg/L	Feb-03-10	APHA 4500-NH3 G	KEL
Nitrogen, Nitrate as N	0.30	MAC = 10	0.01	mg/L	Feb-04-10	APHA 4110 B	KEL
Nitrogen, Nitrite as N	< 0.01	MAC = 3.2	0.01	mg/L	Feb-04-10	APHA 4110 B	KEL
Nitrogen, Total Kjeldahl	0.13		0.05	mg/L	Feb-05-10	APHA 4500-N D	KEL
Nitrogen, Organic	0.13		0.05	mg/L	Feb-05-10	CALC	KEL
pH	7.61	AO = 6.5 - 8.5	0.10	pH Units	Feb-04-10	APHA 4500~H-+	KEL
Phosphorus, Total	< 0.01		0.01	mg/L	Feb-05-10	APHA 4500P:B.5/E	KEL
Solids, Total Dissolved	97	AO ≤ 500	5	mg/L	Feb-08-10	APHA 2540 C	KEL
Sulfate	16.2	AO ≤ 500	1.0	mg/L	Feb-04-10	APHA 4110 B	KEL
Sulfide ,	< 0.050	AO ≤ 0.05	0.050	mg/L	Feb-05-10	APHA 4500-S D	KEL
Temperature	2.4	AO ≤ 15		С	Feb-1.0-10	N/A	KEL
Turbidity	<0.1	Varies, See Guidelini	es 0.1	NTU	Feb-04-10	APHA 2130 B	KEL
UV Transmittance @ 254nm	97.5		0.1	%	Feb-08-10	APHA 5910B	KEL

Total Recoverable Metals by ICPMS

Silverton Well# 2, (Well Tag 27023)	(K0B0153-01)	Matrix: Water	Sampled: Feb	-03-10 08:30			
Aluminum	<0.050	AO ≤ 0.1	0.050	mg/L	Feb-09-10	EPA 6020A	RMD
Antimony	< 0.0010	MAC = 0.006	0.0010	mg/L	Feb-09-10	EPA 6020A	RMD
Arsenic	< 0.0050	MAC = 0.01	0.0050	mg/L	Feb-09-10	EPA 6020A	RMD
Barlum	0.0219	MAC = 1	0.0050	mg/L	Feb-09-10	EPA 6020A	RMD
Beryllium	<0.0010		0.0010	mg/L	Feb-09-10	EPA 6020A	RMD
Boron	0.026	MAC ≈ 5	0.020	mg/L	Feb-09-10	EPA 6020A	RMD
Cadmium	<0.00010	MAC = 0.005	0.00010	mg/L	Feb-09-10	EPA 6020A	RMD
Calclum	27.4		1.0	mg/L	Feb-09-10	EPA 6020A	RMD
Chromium	<0.0050	MAC = 0.05	0.0050	mg/L	Feb-09-10	EPA 6020A	RMD
Cobalt	< 0.00050		0.00050	mg/L	Feb-09-10	EPA 6020A	RMD
Copper	<0.0010	AO ≤ 1	0.0010	mg/L	Feb-09-10	EPA 6020A	RMD
Iron	<0.10	$AO \le 0.3$	0.10	mg/L	Feb-09-10	EPA 6020A	RMD
Lead	<0.0010	MAC = 0.01	0.0010	mg/L	Feb-09-10	EPA 6020A	RMD
Magnesium	3.15		0.10	mg/L	Feb-09-10	EPA 6020A	RMD
Manganese	<0.0020	$AO \leq 0.05$	0.0020	mg/L	Feb-09-10	EPA 6020A	RMD
Mercury	<0.00050	MAC ≈ 0.001	0.00050	mg/L	Feb-09-10	EPA 6020A	RMD
Molybdenum	0.0019		0.0010	mg/L	Feb-09-10	EPA 6020A	RMD
Nickel	<0.0020		0.0020	mg/L	Feb-09-10	EPA 6020A	RMD
Phosphorus	<0.20		0.20	mg/L	Feb-09-10	EPA 6020A	RMD

SAMPLE DATA



CLIENT PROJECT FILE

Vanadlum

Zinc

Topp, Larry

Silverton Well #2

WORK ORDER #

Feb-09-10 EPA 6020A

Feb-09-10 EPA 6020A

K0B0153

RMD

RMD

REPORTED

Feb-15-10

Analyte	Result	Canadian DW Guidelines	RDL	Units	Analyzed	Method	Lab	Notes
		(May 08)	, , , , , , , , , , , , , , , , , , , 	* ****				

Total Recoverable Metals by ICPMS, Continued

Silverton Well# 2, (Well Tag 27023)	(K0B0153-01)	Matrix: Water	Sampled: Feb	-03-10 08:	:30, Continued			
Potassium	1.38		0.10	mg/L	Feb-09-10	EPA 6020A	RMD	
Selenium	< 0.0030	MAC = 0.01	0.0030	mg/L	Feb-09-10	EPA 6020A	RMD	
Silicon	2.5		2.0	mg/L	Feb-09-10	EPA 6020A	RMD	
Silver	<0.00050		0.00050	mg/L	Feb-09-10	EPA 6020A	RMD	
Sodium	1.60	AO ≤ 200	0.10	mg/L	Feb-09-10	EPA 6020A	RMD	
Uranium	0.00188	MAC = 0.02	0.00020	mg/L	Feb-09-10	EPA 6020A	RMD	

AO ≤ 5

0.010 mg/L

0.010 mg/L

Microbiological Parameters

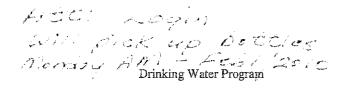
Silverton Well# 2. (Well Tag 27023)	(KOBO153-01)	Matrix: Water	Sampled: Feb-03-10 08-30

< 0.010

0.036

	(
Iron Related Bacteria	<2		2 CFU/mL	Feb-03-10	DBISOP-06	KEL
Sulphate Reducing Bacteria	<8.0		8.0 CFU/mL	Feb-03-10	DBHSOP-05	K£L
Coliforms, Total	<1	MAC < 1	1 ' CFU/100mL	Feb-03-10	APHA 9222	KEL '
Background Colonies	<1		1 CFU/100mL	Feb-03-10	APHA 9222	KEL
E. coli	<1	MAC < 1	1 CFU/100mL		APHA 9223	KEL





PARAMETER LIST FOR NEW DRINKING WATER SOURCES

Evaluating proposed water sources for the presence and concentrations of hazardous organisms/substances and identifying trends in water quality is crucial for the health assessment, source protection planning, and water system design processes. The data required, sampling locations, and frequency of sampling to characterize a proposed source should be established by the design team, but will typically include the following:

BACTERIOLOGICAL:

E. coli

Background growth

Total Coliform

Protozoa

CHEMICAL AND PHYSICAL:

Alkalinity Aluminum Ammonia

Antimony Arsenic

Barium Boron Cadmium

Calcium Chlorides Chromium

Colour Conductivity (Conductance/Specific

Conductance)

Copper

Corrosivity (Calcium

Carbonate saturation/Langelier's

index) Cyanide Fluoride

Hardness Iron Lead

Magnesium Manganese Molybdenum Mercury

Nitrates

Organic Nitrogen

pН

Potassium Selenium Sodium Sulphate

Phosphorous

Sulphide (ground water

sources only) Temperature

Total Dissolved Solids Total Organic Carbon

Turbidity Uranium

UV transmittance

Zinc

*Testing should be done by an approved laboratory with samples collected using appropriate methods.

ADDITIONAL TESTING FOR SPECIFIC CONTAMINANTS

Additional analysis may be required based on the results of the initial analysis and on potential impact by nearby sources of contamination. For example, if industrial, agricultural or forestry contamination (e.g. pesticides) is suspected, identify what chemicals have been used and analyze for the most likely indicator parameters. If petroleum contamination is suspected analyze for BTEX (benzene, toluene, ethyl benzene and xylene) and conduct a hydrocarbon scan.

SEASONABLE VARIABILITY

To provide a reasonable account of seasonal variability source monitoring should typically be carried out over a two year period. The monitoring, including frequency and extent necessary to characterize the source should be made a condition of approval, if acceptance of the source and/or construction permit by Interior Health is granted before the end of the two year period.

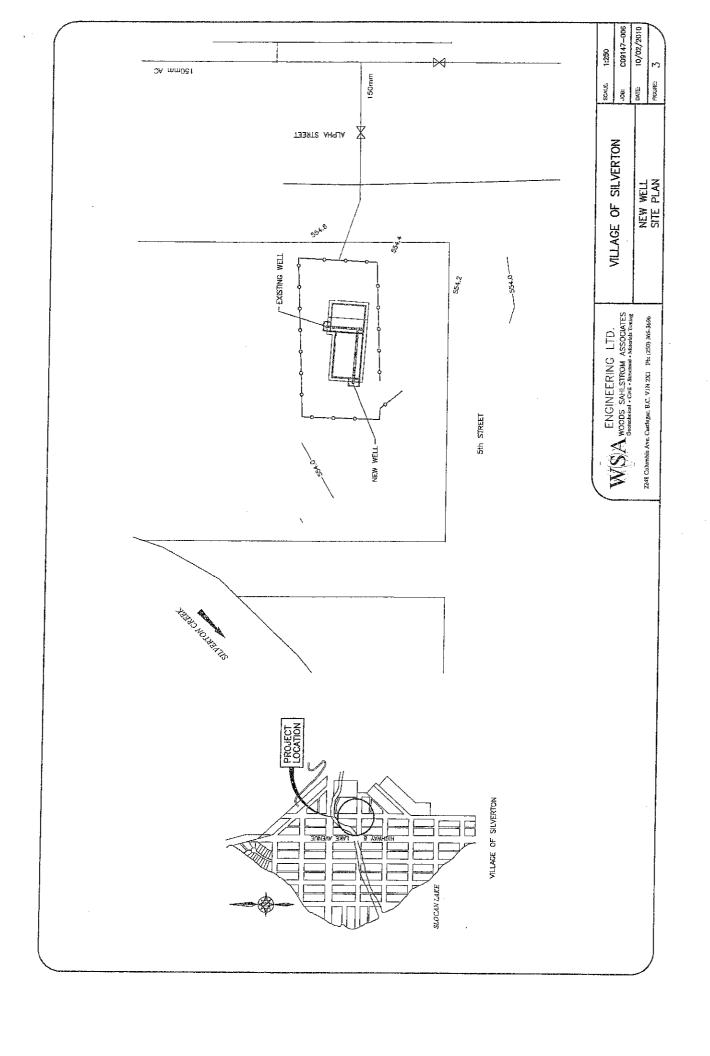
APPENDIX D

IHA Application for New Drinking Water Source



Application for New Drinking Water Source

N		late
	Villages of Silverton Water System	Feb 22/10
St	r r	/
	PO Box 14, 421 Lake Ave.	
Co	12.	ostal Code
	Village of Silverton	
A	phrant Name	
Ar	Village of Silverton	
r		1000
Ph	one(s) Email	G 2250
6	250) 358-2404 Works@ sile	lecton con
Ple	ease provide the following information with the application:	
1.	A site assessment/contaminant survey including a site location map to s	
	proposed source location and distance to buildings, roads, storm sewers	
	water mains, septic tanks, septic fields, water courses such as lakes, rive potential sources of contamination. Please attach map and site survey to	
	form.	tins application
2	A water quality analyses results per HPF10160 "Parameter List for New	, Deinleine Water
44	Sources.	Difficult Mater
3	Is the proposed water source(s) Surface water □ Ground water ☒	Combined [7]
		Combined L
4.	For Surface Water: What is the expected depth of the intake?	
5.	For Ground Water:	
6.	What is the expected depth to the well screen?	136 ft (41.5 m)
7.	Is it expected that there will be a clay layer or impervious layer above	
	the above the well screen or intake?	🛛 Yes 🛚 No
8.	Is it expected that the aquifer will be artesian?	🗆 Yes 💆 No
Sub	omitted by:	
***	Topp, F. Gao.	77)
		1. 20 001=
Sigt	fature of the state of the stat	Date 2010



November 3, 2009

32900-20/ Village of Silverton - Log 619

Ralf Waters, P.Eng. WSA Engineering Ltd. 2248 Columbia Avenue Castlegar, BC V1N 2X1

Dear Mr. Waters:

Re: Application for Construction Permit – Village of Silverton – Pump House Piping Upgrade to Connect New Well Source

Thank you for the Construction Permit application and drawings received October 20, 2009 for the construction of waterworks for the above mentioned project. At this time we are unable to issue a construction permit as no approval or acceptance have been issued by Interior Health for a new well source for the Village of Silverton.

Please find enclosed the applications and information for obtaining a new source. This approval/ acceptance is not only for the source water quality but acceptance of the proposed well site, i.e. in an acceptable location. In discussion with the Environmental Health Officer, Paul Geisler, he advised that there were some preliminary discussions regarding a proposed new well source, but at the time a site was not selected. This process is conducted prior to the drilling of a new well.

Please ensure your client, the Village of Silverton, completes the new source acceptance/ approval process. Once the source site and the source quality have been accepted by the Environmental Health Officer we will be able to consider the application for the works to connect the new well source to the existing water system. From the drawing submitted, some preliminary items noted for the proposed well source which should be addressed are proximity to the existing well source and building and proximity to a surface source. Other items are provision for flushing the well as may be required from time to time and ability to sample raw water quality.

Please re-apply when the new source acceptance/ approval process has been satisfied. Please refer to our Waterworks Construction Permit Guidelines for the documentation required when submitting an application for a new well source being connected to a water system.

Please contact the undersigned if you have any questions.

Yours truly,

C.C.

Marianne Crowe, P. Eng. Public Health Engineer Kootenay Region

Paul Geisler, EHO, IHA, 2nd Floor, 333 Victoria Street, Nelson, BC, V1L 4K3 Village of Silverton, PO Box 14, 421 Lake Ave, Silverton, BC, V0G B0 Ministry of Community Services, Municipal Engineering Services Branch, PO Box 9838 Stn Prov Govt, Victoria, BC, V8W 9T1 File

NEW DRINKING WATER SOURCE GUIDELINE

1.0 INTRODUCTION

Health Protection staff engage in assessing and evaluating proposed new sources of drinking water to ensure they are properly located and verify possible sources of contamination or drinking water health hazards.

The guideline outlines evaluation information necessary to assess health risks, support source protection efforts, and facilitate proper system design. Surface and ground water source components include:

1.1 Surface Water Sources

- a) Watershed characterization (e.g. hydrology, water quality, trends).
- b) Contaminant survey results that identify hazards in a watershed and have the potential to impact water quality.
- c) Risk characterization including consequences to drinking water.
- d) Source protection measures to be considered or implemented.

1.2 Ground Water Sources

- a) Aquifer characterization (e.g. well site selection, aquifer vulnerability)
- b) Contaminant survey results that identify hazards that may impact well water quality.
- c) Risk characterization including consequences to drinking water.
- d) Identification of wellhead protection measures to be considered or implemented.

2.0 PROCESS

*Note: An Application for New Drinking Water Source must be submitted to the local Environmental Health Officer prior to submitting an Application for Waterworks Construction Permit to Public Health Engineering.

- 2.1 The applicant on behalf of a water supply system proposing a new drinking water source provides the following to the local Environmental Health Officer (EHO):
 - a) A completed HPL0940 Application for New Drinking Water Source including:
 - Water system name, legal owner, address, phone number
 - location, nature and type of proposed source
 - · water quality analyses results

- b) Results from a site inspection and contaminant survey. For guidance regarding the evaluation of proposed surface or groundwater sources please refer to HPF10140 Evaluation Criteria for Surface Water or HPF10150 Evaluation Criteria for Ground Water respectively.
- 2.2 The Environmental Health Officer is responsible for the following:
 - a) When a completed HPL0940 Application for New Drinking Water Source is received the EHO initiates the review and evaluation process.
 - b) Originals of the application and supporting information are kept by the Environmental Health Officer. Copies of information are provided to appropriate staff as required. Examples are the Drinking Water Specialist, Team Leader, and Source Protection Officer.
 - c) As part of the source assessment process, evaluate the appropriateness of the proposed water source by:
 - Carrying out a site inspection of the proposed source prior to the construction of any works (i.e. intake or well).
 - Reviewing a water quality analyses with reference to the *Drinking Water Protection Act* (DWPA), Guidelines for Canadian Drinking Water Quality (GCDWQ), and Ministry of Environment Source Water Quality Guidelines.
 - Consulting with members of the Drinking Water Team (e.g. Public Health Engineer, Medical Health Officer, Drinking Water Specialist, and Source Protection Officer) as required.
 - d) Upon completion of the evaluation process the Environmental Health Officer will forward site inspection results and water quality evaluation to the water system applicant (a copy is provided to the Public Health Engineer). They will indicate whether the proposed source is appropriate to be considered for use as a drinking water source (i.e. can or can not be used), whether treatment is required, and identify any other concerns they may have regarding the proposed drinking water source.

EVALUATION CRITERIA FOR NEW DRINKING WATER GROUND WATER SOURCES

1.0 INTRODUCTION

The intent of the source assessment process is to provide the information necessary to evaluate potential health risks, support source protection planning, and facilitate proper system design. The information provided should include the following elements:

- 1. Source assessment (e.g. well site selection)
- 2. Identification of potential sources of contamination that may impact water quality
- 3. Identification of wellhead protection measures to be considered or implemented.

2.0 INVESTIGATION CRITERIA

The depth of investigation and amount of information required to support system design will vary for each situation.

- a) Water systems proposing to service >500 persons should typically be expected to complete an assessment equivalent to that described in modules 1, 2, & 7 of the BC Comprehensive Source-to-Tap Assessment Guideline (see references).
- b) Small water systems (i.e. those serving <500 persons) should at a minimum provide an assessment equivalent to that described in the BC Drinking Water Source-to-Tap Screening Tool (see references)
- c) Considerations:

The following items may be considered during the site assessment of a proposed surface drinking water source. This list is not exhaustive, but is intended to stimulate thought:

Does the water supplier	own the la	nd that the pro	mosed well will be			
located on?	OWN INC III	na mat mo pro	phosed wen will be	☐ Yes	□ No	
Is the aquifer in the gene	****					
(MOE website-Wells, A	-		• •	□ Yes	□ No	
Does the proposed well I GUDI/GWUDI?	☐ Yes	□No				
Are there any contamina	the proposed well					
location? (MOE contami	location? (MOE contaminated sites registry)					
Is any of the following o well?	ccurring w	rithin the capt	ure zone or within 100m	of the prop	osed	
Cattle Grazing	☐ Yes	□ No	Agriculture	□ Yes	□ No	
Fertilizer Use	□ Yes	□ No	Industrial .	☐ Yes	□ No	
Fuel storage	Fuel storage					
Manure Stockpiles	Stockpiles				□ No	
Salt storage	□ Yes	□ No			-	

HPF10150 January 2009

Interior H Health Pr	lealth otection Manual	Drinking Wate	er Program
Are	e there any sewerage disposal systems within 30 metres?	☐ Yes	□ No
	e there any Municipal Sewage Regulation disposal systems within 9 tres?	0 □ Yes	□ No
Are	e there any cemeteries within 120 metres?	☐ Yes	□ No
- 1	he area low lying or potentially subject to flooding (i.e. within the 2 or flood level)?	.0 □ Yes	□ No

3.0 REFERENCE DOCUMENTS

No one process for assessing ground water will be appropriate for all systems. However, the following provincial documents provide some guidance regarding the collection of information to support water system design:

- a) BC Drinking Water Source-to-Tap Screening Tool (Section B1) (www.health.gov.bc.ca/protect/source.html#water2)
- b) BC Comprehensive Source-to-Tap Assessment Guideline (Modules 1, 2, & 7) (www.bcwwa.org/source-to-tap/index.php)
- c) BC Well Protection Toolkit (www.env.gov.bc.ca/wsd/plan protect sustain/groundwater/wells/well protection/well protect.html)

More extensive lists of hazards and elements to be considered can be found in the:

- d) BC Well Protection Toolkit (Appendix 3.1),
- e) Guidance Document for Determining Ground Water at Risk of Pathogens and Ground Water Under Direct Influence of Surface Water (Province of BC Draft Document),
- f) CCME's From Source to Tap: Guidance on the Multi-barrier Approach to Safe Drinking Water (www.ccme.ca/publications/list_publications.html),
- g) USEPA Source Water Protection website (http://cfpub.epa.gov/safewater/sourcewater/):